

Background

Multi-robot systems demonstrate great potential for a wide range of applications, from disaster relief, to interplanetary exploration, to improving industrial warehouse efficiency. The operational time of existing mobile robotic systems, however, is limited by finite battery life. Existing solutions have limitations:

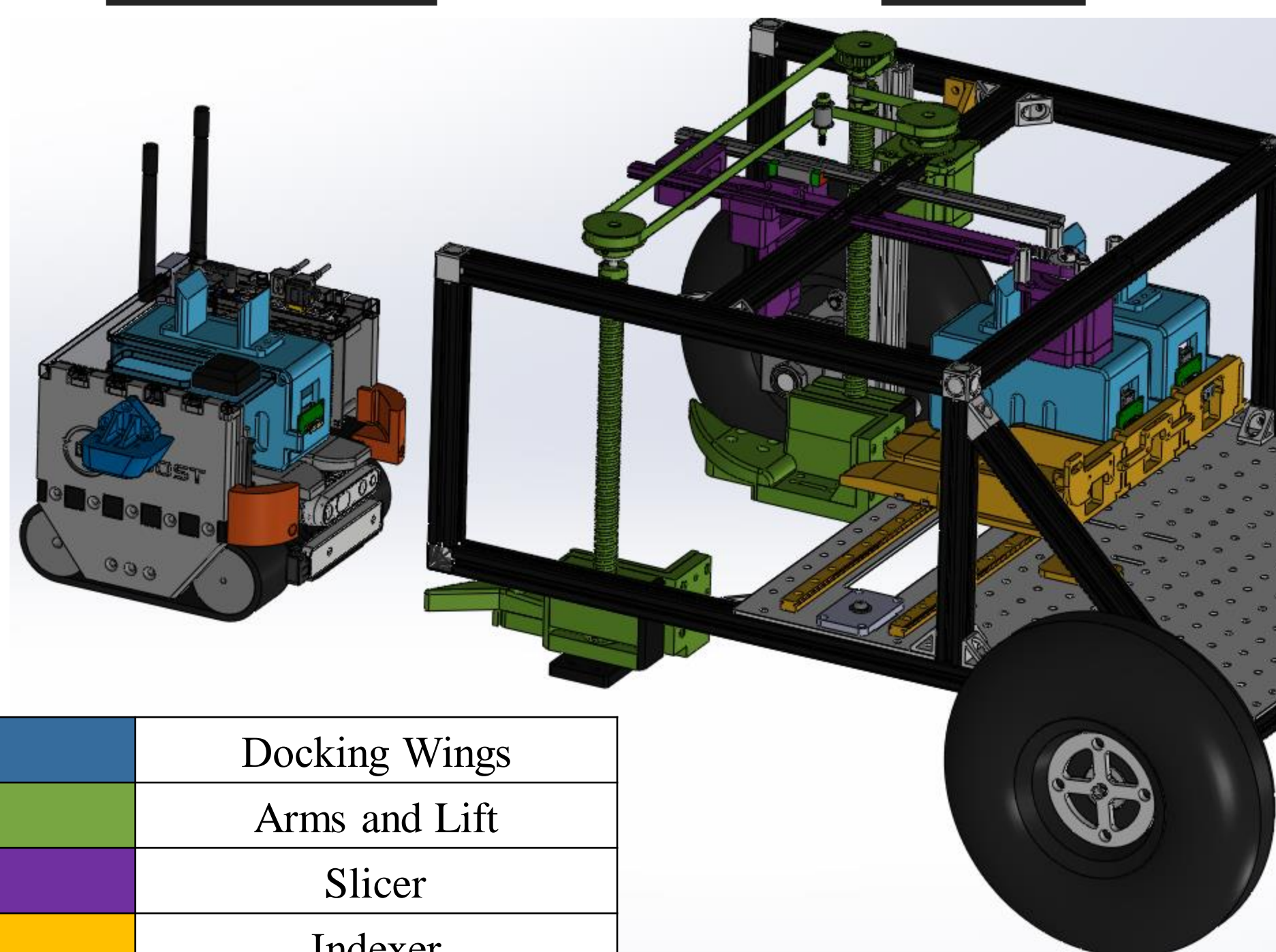
Solution	Limitation
On-Board Power Generation	Poor Scaling
Tethered Power	Limits Operational Range
Charging	Long Robot Downtime
Human Intervention	Undermines Autonomy






Problem Statement

To design a multi-robot architecture that overcomes the limitations of finite battery life and is capable of operation over uneven terrain.

Design Overview

2x Minibots 1x Hub



	Docking Wings
	Arms and Lift
	Slicer
	Indexer
	Battery Module
	Minibot Bumpers

Battery Swap Procedure

- Hub charges battery modules with its own supply.
- Minibot explores until it is low on battery.
- Minibot drives into hub dock. Docking arm and bumpers assist initial alignment.
- Docking arms lift minibot into position for battery swap.
- Slicer moves battery module between minibot and hub.
- Indexer moves battery cache to receive or send off.

Constraints:

- Dock and swap battery on unknown terrain
 - Docking must account for mechanical misalignment in 6 DOF for both hub and minibot
- Battery swap must be quick and reliable
- Emphasis on scalability

Entry Lead-In Optimization

Purpose:

Verify and optimize geometry of docking receivers and minibot bumpers to maximize successful entry regardless of entry vector

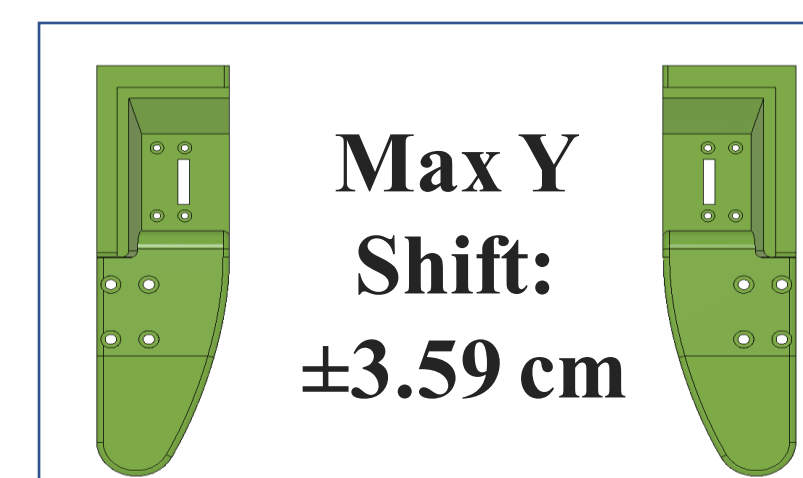
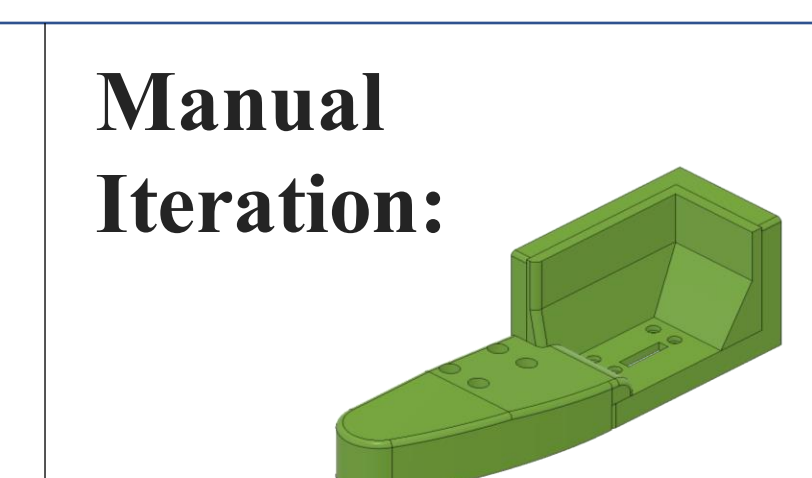
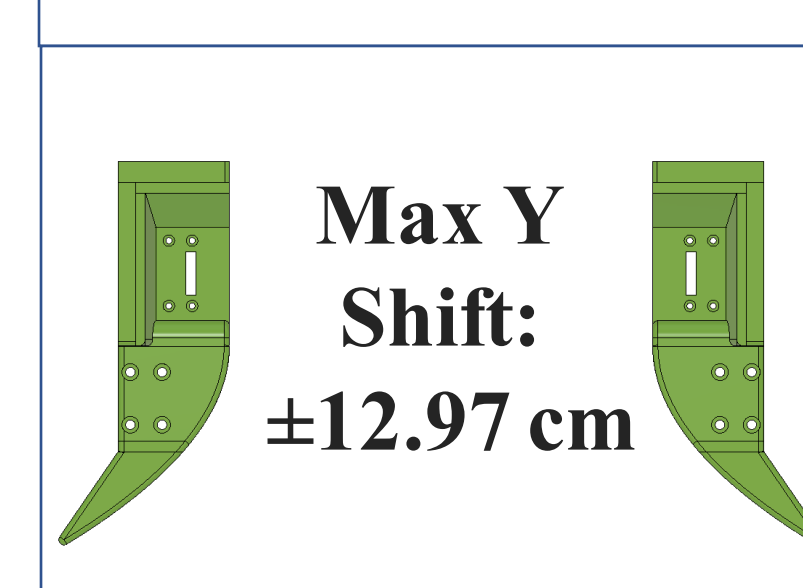
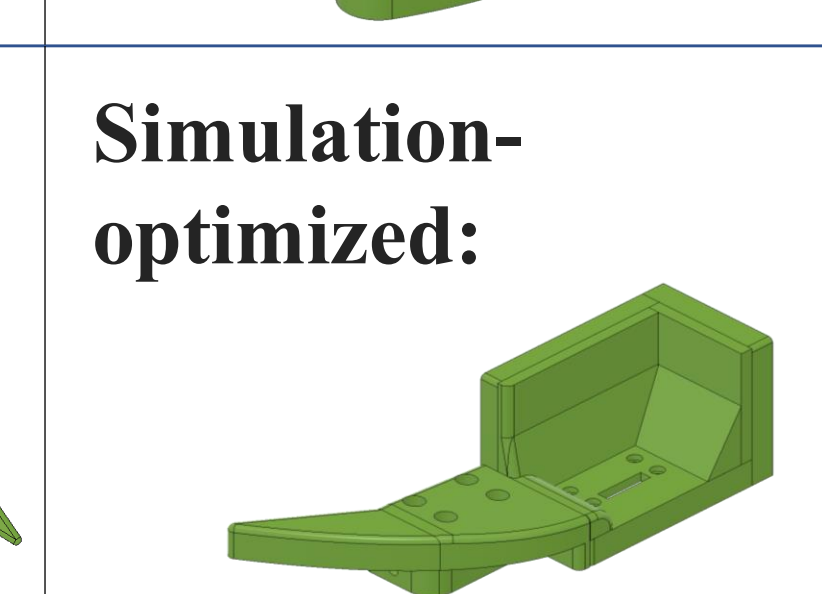
Analysis:

Simulated minibot entry for hundreds of randomized starting positions to find performance rate using Monte Carlo design

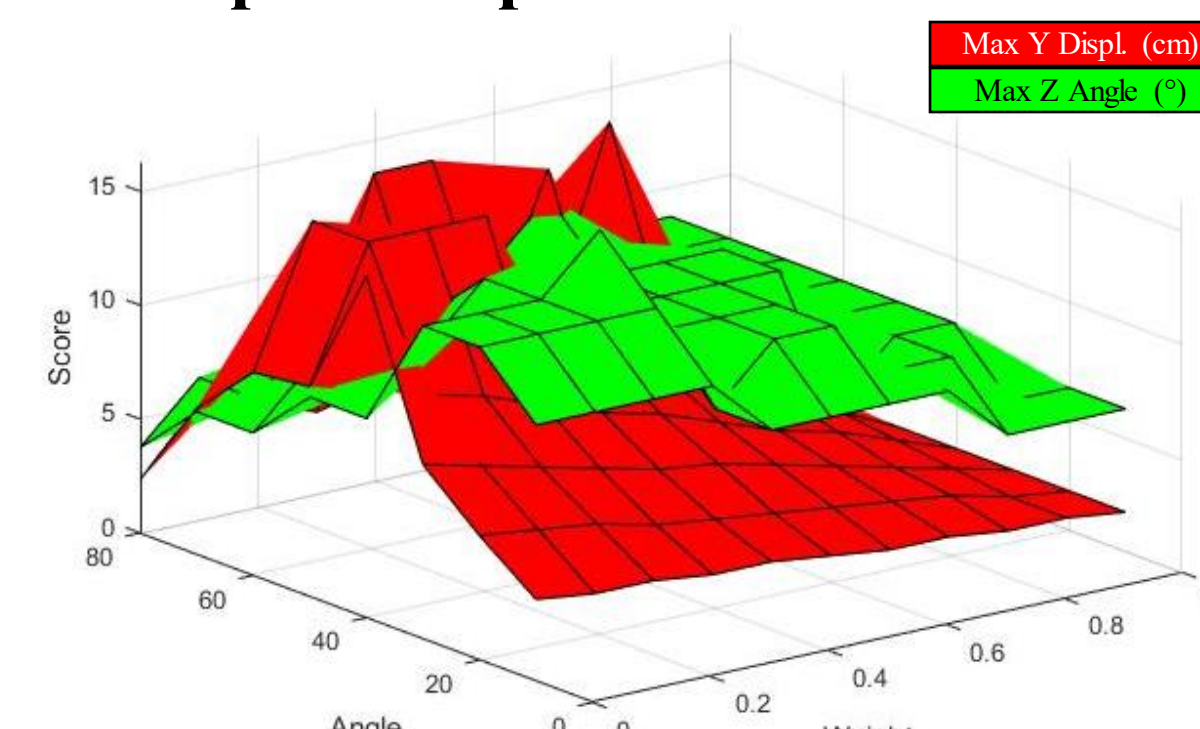


Impact:

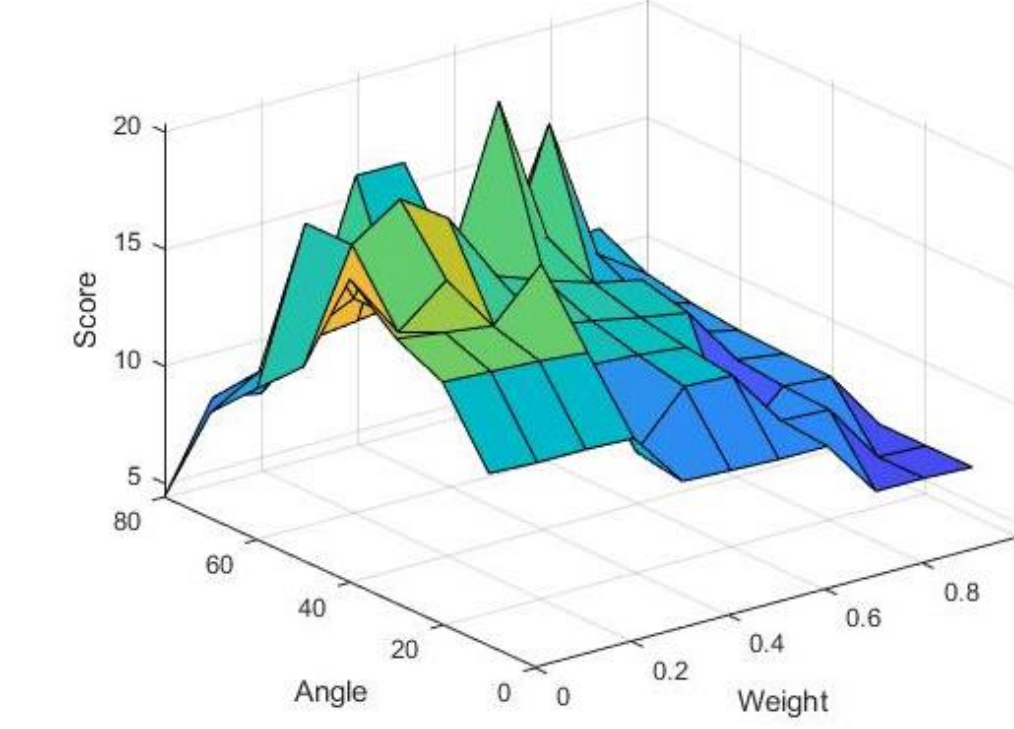
Implemented bumpers on minibot and verified performance of optimized lead-ins on arms.

	Max Y Shift: ±3.59 cm	Manual Iteration:	
	Max Y Shift: ±12.97 cm	Simulation-optimized:	

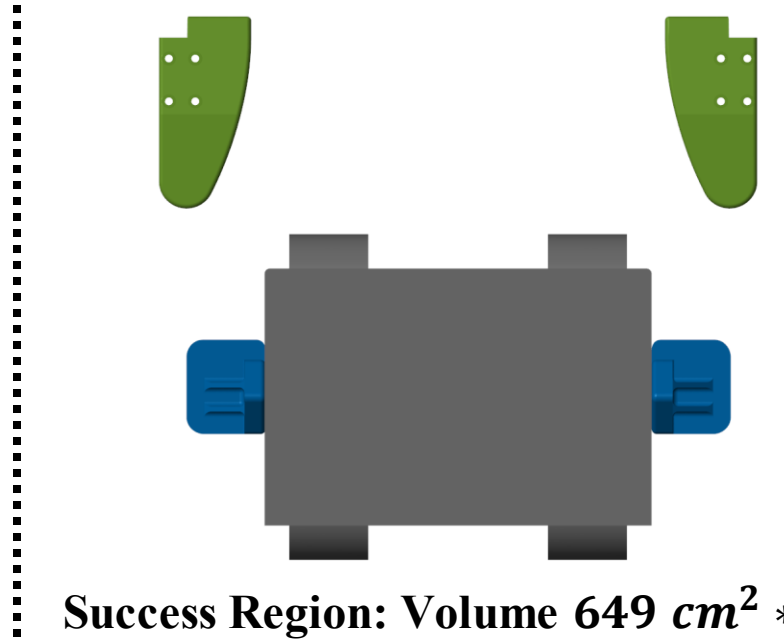
Optimal Spline Grid Search:



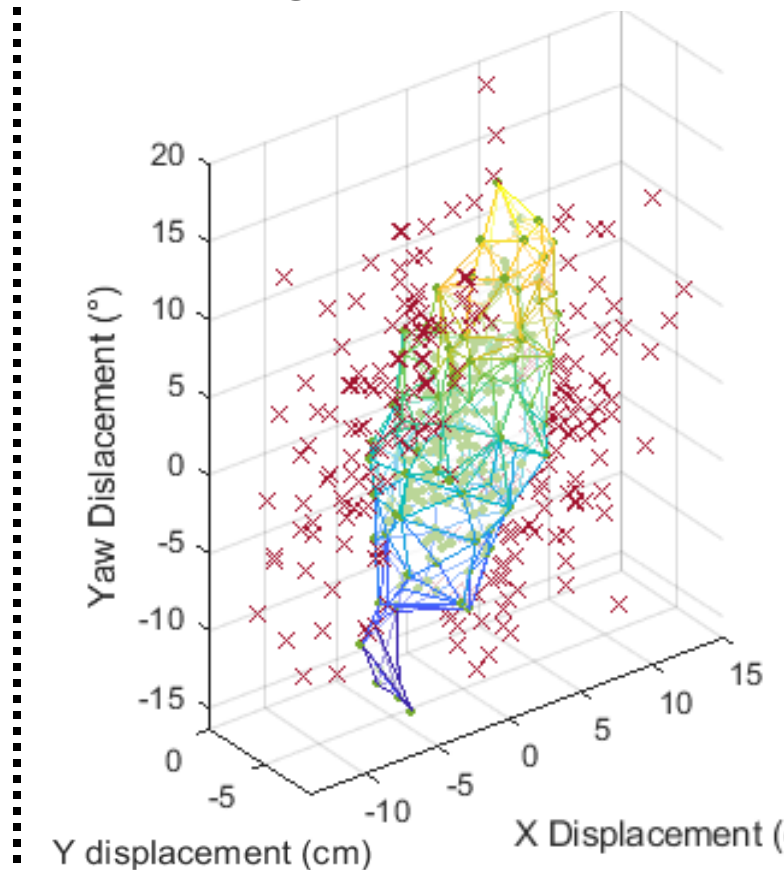
Root-Sum-Square Scores:



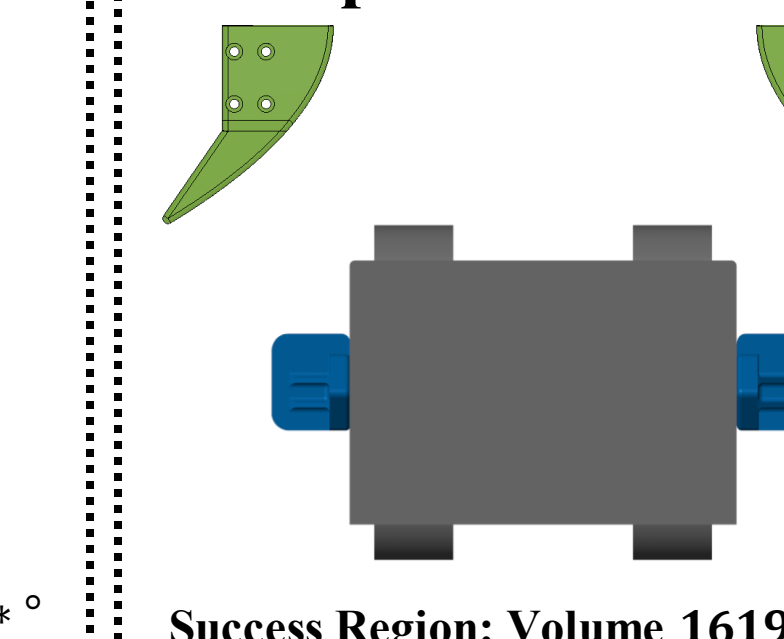
Manual Iteration



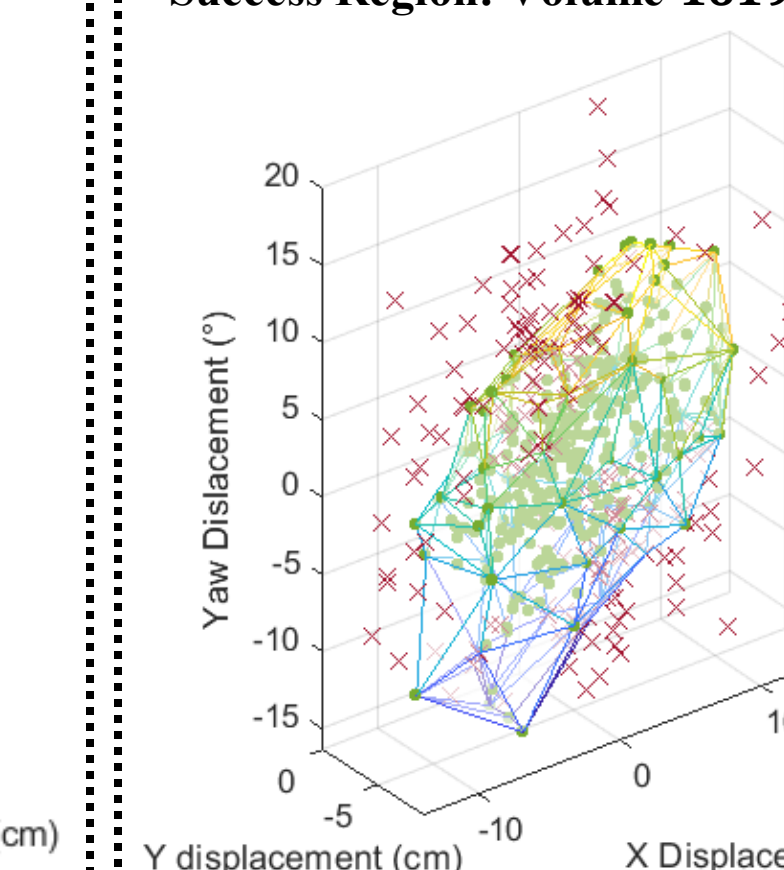
Success Region: Volume 649 cm² *



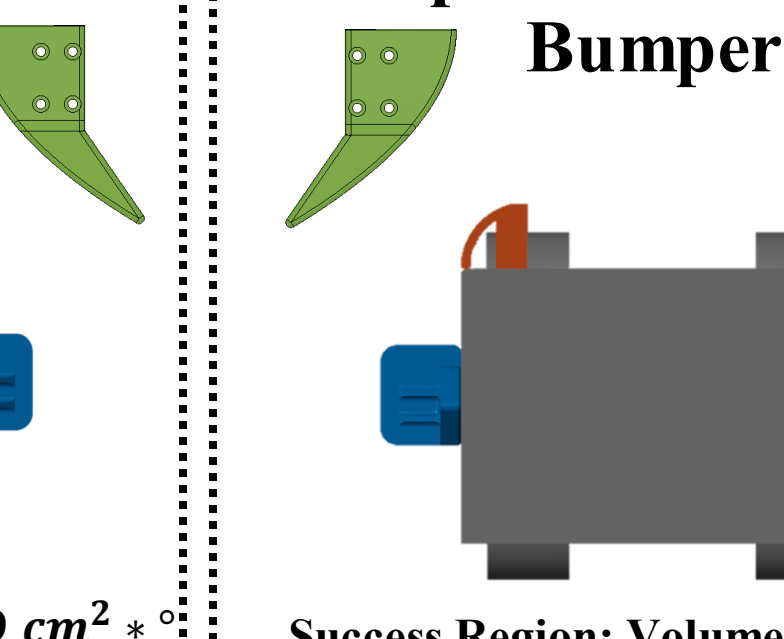
Optimized Arms



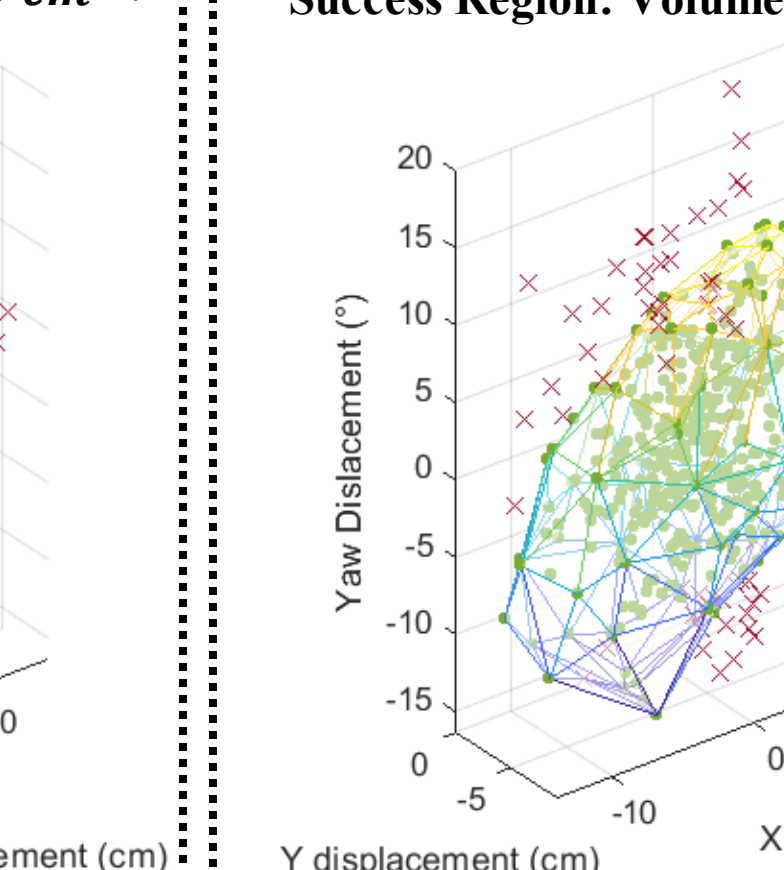
Success Region: Volume 1619 cm² *



Optimized Arms + Bumpers



Success Region: Volume 2327 cm² *

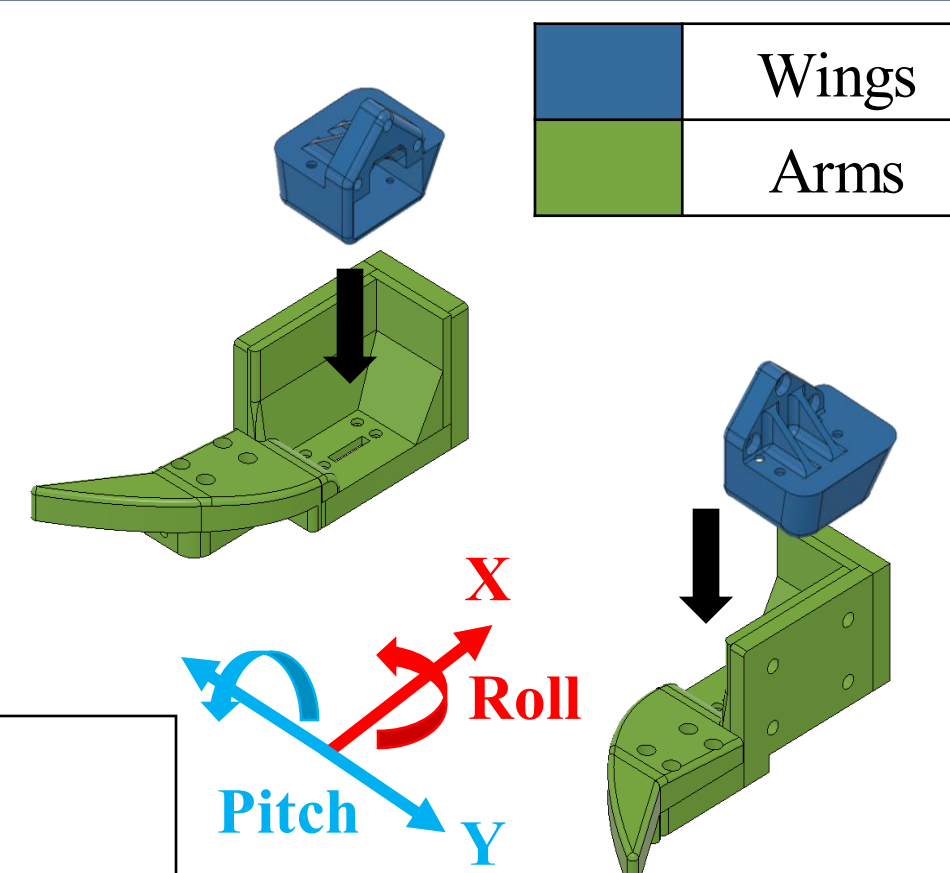


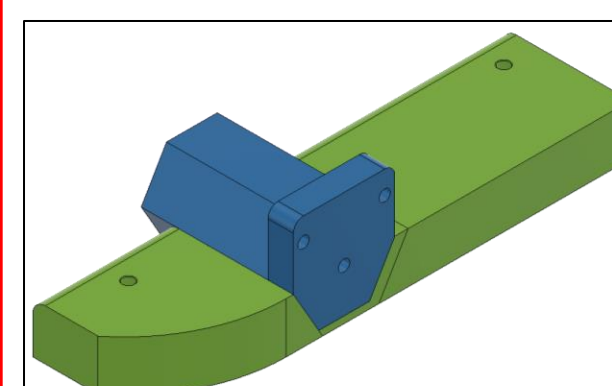
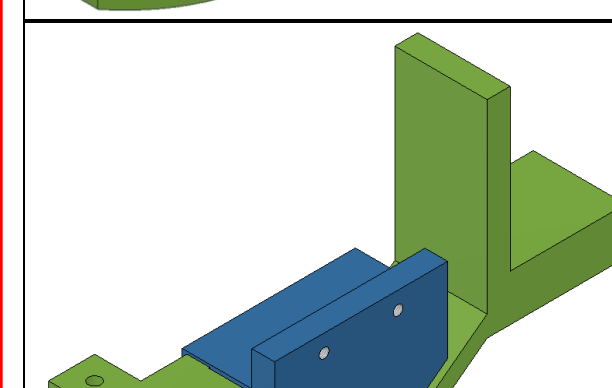
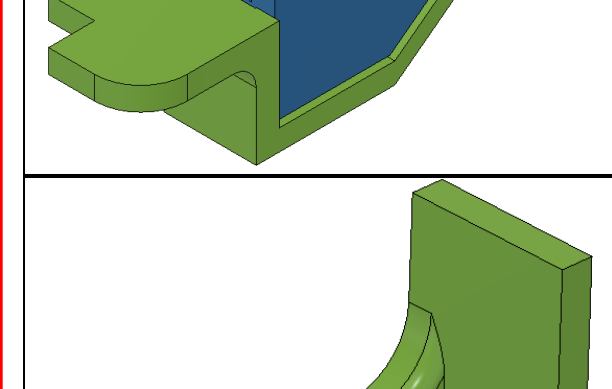
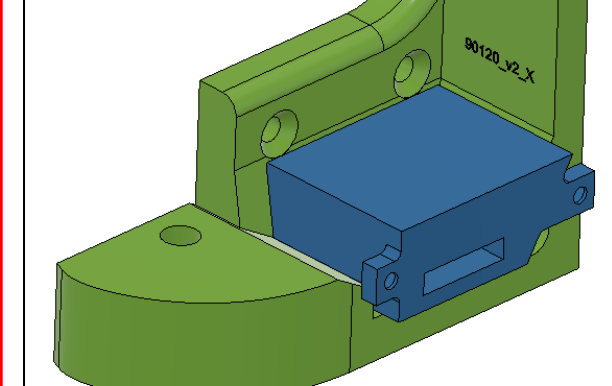
258.6% Volume Compensation Increase

Lifting Misalignment

Purpose:

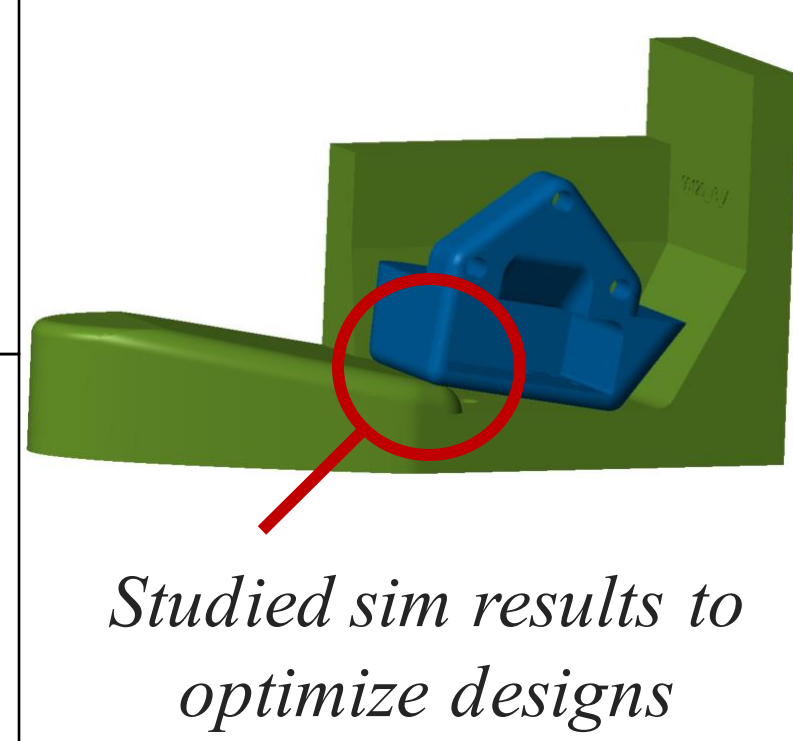
Optimize wing and arm mating geometry to account for ± 5° and ± 5 mm misalignment in 6 DOF



	Series 1: <ul style="list-style-type: none"> Easy overshoot x Unconstrained in y Small area of engagement
	Series 2: <ul style="list-style-type: none"> Hard stop fixes overshoot in x Profile resolves roll
	Series 3: <ul style="list-style-type: none"> Side wall constrains y and correct pitch Over-constrained edges cause jamming
	Series 4: <ul style="list-style-type: none"> Optimized using simulation performance

Simulated a Fractional Factorial Experimental Design

Efficiently investigates the effects of combined misalignment without testing thousands of combinations.



Final wing and arm design passes all ± 5° and ± 5 mm combined misalignments explored in simulation!

Motor and Structural Analysis

Stepper Motor Selection by Required Torque

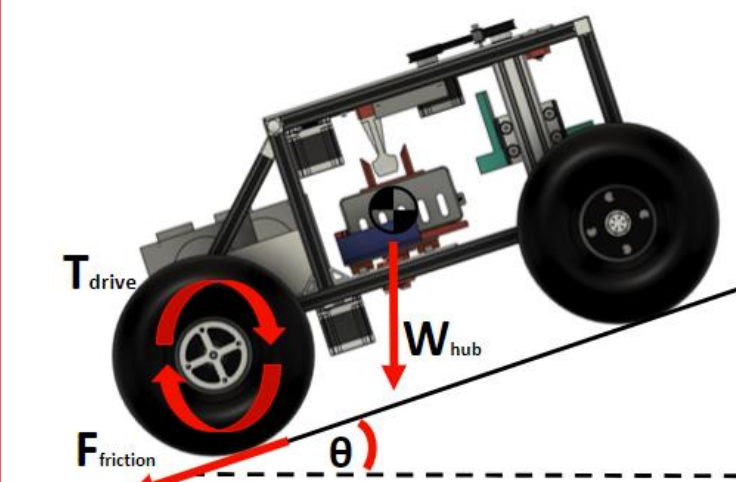
Required Torques:
 Lifting: 0.0179 N·m
 Slicer: 0.0445 N·m
 Indexer: 0.1226 N·m

$$T_R = \frac{F \cdot d_m}{2} \cdot \left(\frac{L + \pi \cdot \mu \cdot d_m}{\pi \cdot d_m - \mu \cdot L} \right)$$

Selected Nema 23
 Holding Torque: 1.26 N·m

Driving Motor Selections

Most conservative drive case: accelerate from rest up 10° incline.



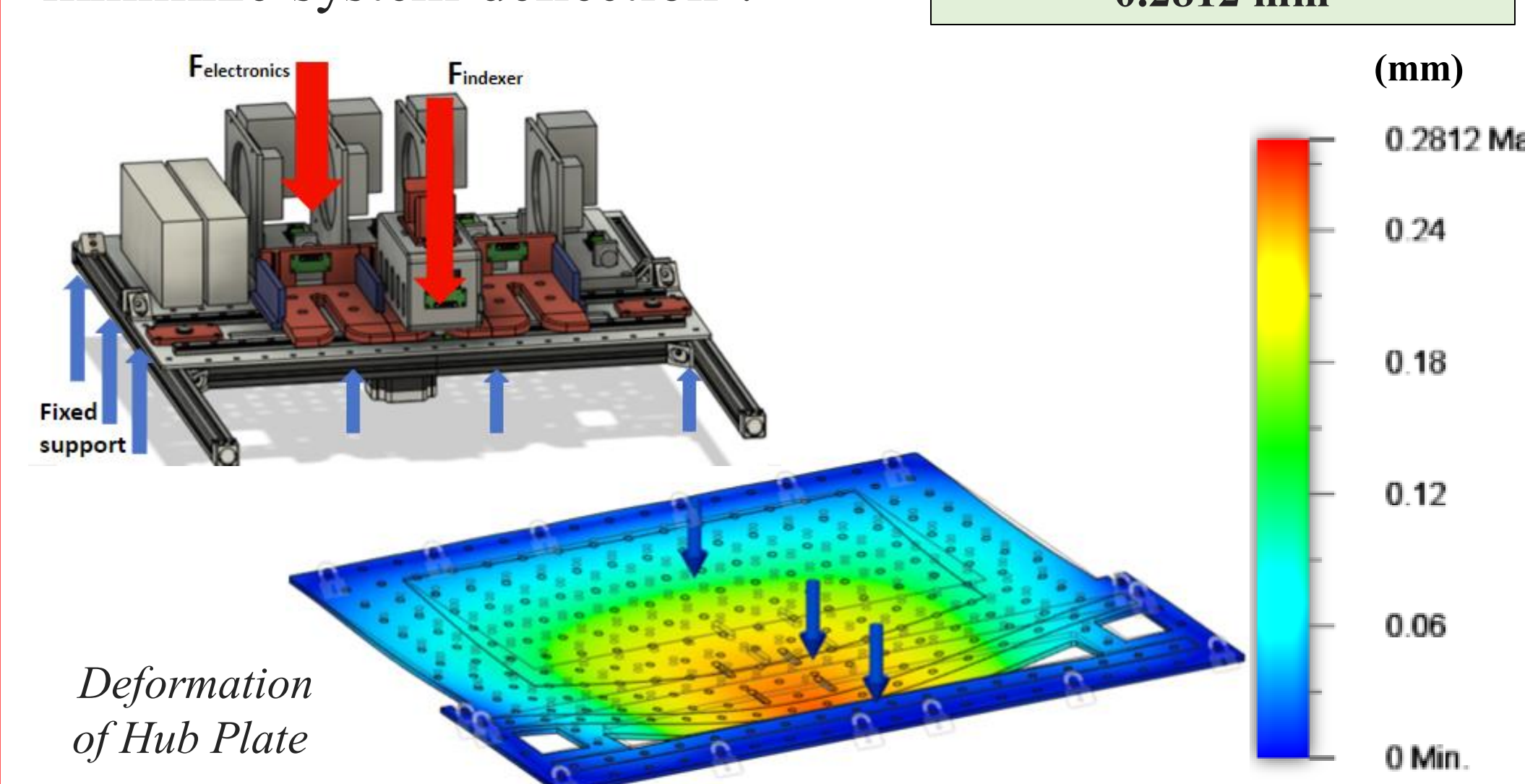
	Minibot	Hub
Drivetrain Torque (N·m)	0.91	28.0
Gearing Ratio (N·m)	1	7
Torque Margin	0.636	1.578

Hub Plates analyzed for bending with conservative loads to minimize system deflection.

FEA

F.S. Yield Safety = 10.6

Maximum Deflection: 0.2812 mm

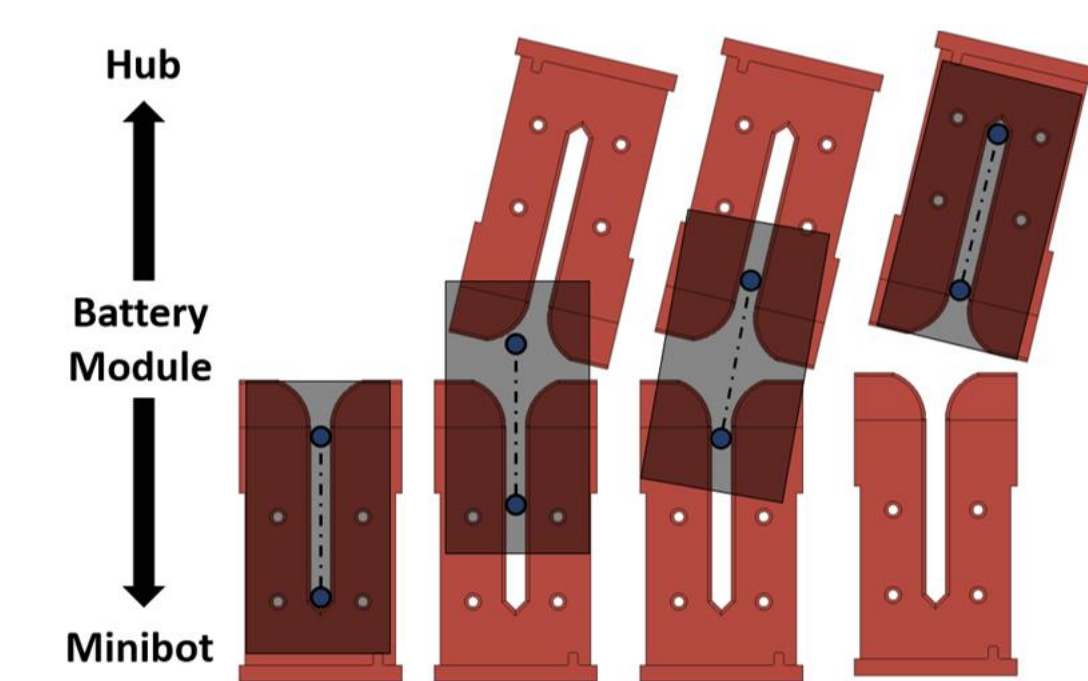


Design Validation

Battery Swap Reliability Tests:

Conducted 50 consecutive, autonomous battery swaps on flat terrain

100% Success Rate



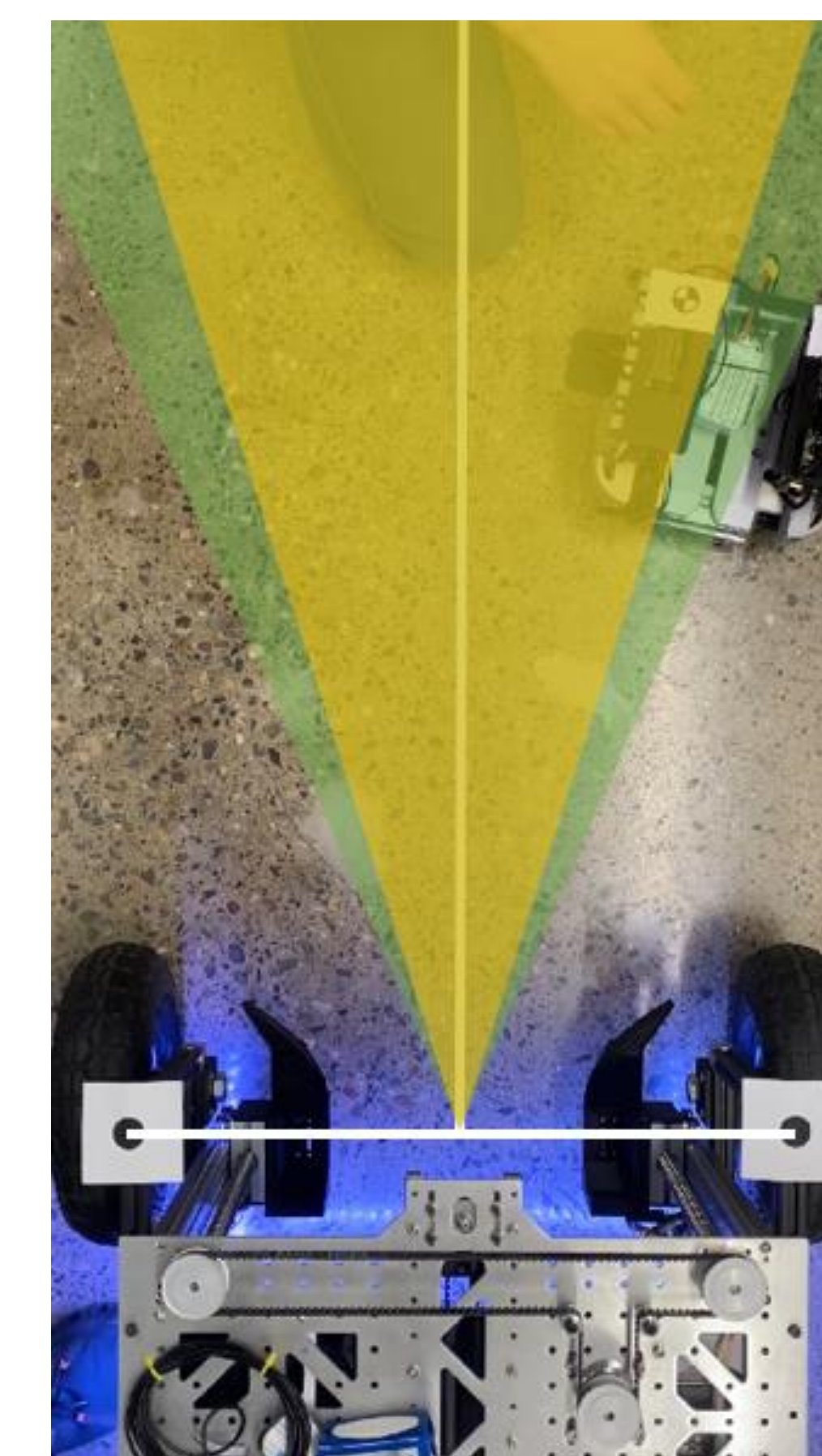
Real-World Lifting Misalignment Verification:

Repeated fractional factorial combined misalignment conditions from simulation on real-world test rig with optimized design

Hub Pitch (deg)	Hub Roll (deg)	MB Pitch (deg)	MB Roll (deg)	MB y (mm)	MB x (mm)	Yaw (deg)	Sim	Real
0	0	5	5	0	5	0	PASS	PASS
5	0	0	5	0	0	5	PASS	PASS
0	0	0	0	5	5	5	PASS	PASS
5	0	5	0	5	0	0	PASS	PASS
0	5	5	0	0	0	5	PASS	PASS
5	5	0	0	0	5	0	PASS	PASS
0	5	0	5	5	0	0	PASS	PASS
5	5	5	5	5	5	5	PASS	PASS

PASS

Real-World Entry Verification:



- Minibot placed in variety of initial positions and drove straight into hub docking port
- Using Canny edge algorithms, minibot position tracked and analyzed in MATLAB

System Yaw Allowance:
 With Software Navigation: ± 23.72°
 Purely Mechanical: ± 17.72°

Future Work

- Continue full-system characterization and publish results
- Implement fatigue simulation to determine max cycles
- Redesign interfaces to improve sand and dust shielding
- Continue discussions with NASA JPL and other robotics companies for future R&D

Inclusivity in Design: Our project lowers the barrier to entry for scalable mobile robotics in applications such as assisted living

Acknowledgements

EECE Team: David Antaki, Jarrod Homer, Musheera Khandaker Maulik Patel, & Ben-oni Vainqueur
 Advisors: Professor Jaeger-Helton, Patrick DeGrosse Jr., Professor Bahram Shafai